

## Theoretical investigation of thermal disorder in CuCo alloys

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### ABSTRACT

In this work, we investigate thermal disorder in intermetallic CuCo alloys by extending the anharmonic correlated Einstein model in extended X-ray absorption fine structure (EXAFS) theory. The expressions of bond-stretching force constants, Einstein frequency and temperature, the atomic mean-square relative displacement characterizing the EXAFS Debye–Waller factor have been derived in terms of Morse potential parameters. We perform numerical calculations for CuCo alloys up to temperature 800 K to study the temperature effects on these thermodynamic quantities. Our research shows that Co–Co bonds are stiffer than Cu–Cu bonds. This leads to the atomic mean-square relative displacement curve of CuCo alloys is lower than the one of Cu metal, but higher than the one of bulk Co. The increasing of Co concentration in CuCo alloys will make the increasing of thermal disorder in the alloy system. Moreover, the dynamic disorder caused by thermal lattice vibrations gives significant contribution to the EXAFS Debye–Waller factor at high temperature.

### 1. Introduction

The binary CuCo alloys recently attract the attention of widespread research community due to their interesting physical properties such as isotropic giant magnetoresistance [1], superparamagnetism [2], spin-glass-like behavior [3], high strength nanocrystalline [4], and the kinetics of growth of nanocrystalline grains [5]. CuCo alloys turn out as an immediate choice for industrial applications because of the relative abundance and low cost of copper and cobalt metals. At ambient conditions, Cu is in face-centered cubic (FCC) structure, while Co is a hexagonal close packed (HCP) metal. By magnetron sputtering CuCo crystalline alloys were observed remaining single FCC phase up to 80% concentration of cobalt metal [6]. Using rapid quenching techniques, Klement reported a single phase FCC solid solution of copper and cobalt in (0–15) and (75–100) at.% Co ranges [7].

Although many studies have been performed to investigate structural evolution [8], magnetic and transport properties [1,2,9] of CuCo alloys, there are only several works regarding to the thermal disorder in the intermetallic CuCo alloys. Indeed studying this fact in detail is a fundamental for developing magneto-caloric applications [10]. The magnetoresistive effect is not only strongly dependent on the size of magnetic particles but also the thermodynamic treatments controlling the microstructural evolution of the alloy. Thermal disorder effect

causes the expansion of atomic positions in crystals which leads to a non-Gaussian distribution of interatomic distances [11,12]. Extended X-ray absorption fine structure (EXAFS) is one of the effective methods for the investigation of structure and thermal disorder of crystalline as well as amorphous materials [13,14]. In order to analyze the thermal lattice vibration effects on EXAFS oscillation, the cumulant expansion approach was presented [15]. In this approach, the second cumulant  $\sigma^2$  corresponds to the parallel mean-square relative displacement (MSRD) of the bond between absorber and backscatterer atoms. It describes the variance of distance distribution function. This parameter affects sensitively on amplitude of EXAFS through the factor  $W(k) = \exp(-2\sigma^2 k^2)$  (where  $k$  is the wavenumber) [16], and then is so-called the EXAFS Debye–Waller factor (DWF). Theoretically, the EXAFS DWF is defined as

$$\sigma^2 = \left\langle \left[ \vec{R} \cdot (\vec{u}_i - \vec{u}_0) \right]^2 \right\rangle = \langle u_i^2 \rangle + \langle u_0^2 \rangle - 2 \langle u_i u_0 \rangle \quad (1)$$

where  $\langle u_i^2 \rangle$  and  $\langle u_0^2 \rangle$  are uncorrelated mean square displacement (MSD) of the *zeroth* and the *i*th atoms, respectively; the term  $2 \langle u_i u_0 \rangle$  is the parallel displacement correlation function (DCF); and  $\vec{u}_0$  and  $\vec{u}_i$  are the atomic displacements of the *zeroth* and the *i*th sites from their

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equilibrium positions;  $\vec{R}$  is the unit vector at the *zeroth* site pointing towards the *i*th site, and the brackets stand for the ensemble averaging.

In present work, we investigate the thermodynamic properties of CuCo alloys based on the anharmonic correlated Einstein model (ACEM) [17] in EXAFS theory. We assume that intermetallic CuCo alloys remain stable in FCC structure with any cobalt composition. Main aim of the present work is to develop the ACEM for binary alloys to derive the interatomic effective potential, bond-stretching force constants, Einstein frequency and temperature, and parallel MSR D characterizing for EXAFS DWF. The temperature effects on Einstein frequency and temperature, EXAFS DWF and related thermodynamic quantities are considered by performing numerical calculations for CuCo alloys up to temperature of 800 K which is below the melting temperatures of Cu and Co metals [18,19] using the pair interaction Morse potential.

## 2. Theoretical approach

### 2.1. Anharmonic correlated Einstein model

Firstly, we make a brief report of the ACEM [17] and its application for FCC and HCP structures. This model is the extension of the correlated Einstein model in order to include the anharmonicity contributions to EXAFS cumulants. In this model, a local vibration picture of absorber and back-scatterer is considered. The author proposed an anharmonic interatomic effective potential  $V_{eff}$  that includes the interactions between absorbing and back-scattering atoms and their nearest-neighbors. Because of the asymmetry of the potential, the effective potential  $V_{eff}$  is expressed as a function of the thermal expansion  $x = r - r_0$  along the bond direction as

$$V_{eff}(x) = \varphi(x) + \sum_{j \neq i} \varphi \left( \frac{\mu}{M_i} x \hat{R}_{AB} \hat{R}_{ij} \right); \quad \mu = \frac{M_A M_B}{M_A + M_B} \\ \approx \frac{1}{2} k_{eff}^0 x^2 + k_3^0 x^3 + \dots \quad (2)$$

where  $r$  and  $r_0$  are, respectively, the instantaneous and equilibrium bond length between absorbing and back-scattering atoms;  $\varphi(x)$  describes the interaction between absorber and backscatterer. The influence of the neighboring atoms to the oscillation of absorber and back-scatterer is characterized by term  $\sum_{j \neq i} \varphi \left( \frac{\mu}{M_i} x \hat{R}_{AB} \hat{R}_{ij} \right)$ , where the sum  $i$  is over absorber ( $i = A$ ) and back-scatterer ( $i = B$ ), and the sum  $j$  is over all their nearest-neighbor atoms, excluding the absorber and back-scatterer themselves; masses of the absorbing and back-scattering atoms are denoted by  $M_A$  and  $M_B$ , correspondingly;  $k_{eff}^0$  and  $k_3^0$  are, respectively, the effective and cubic bond-stretching force constants caused by an asymmetry in the pair distribution function because of thermal disorder.

Originally, the ACEM was developed for pure crystalline materials [17]. For FCC and HCP crystals, each atom is bonded to twelve nearest-neighbor atoms. Applying the ACEM for these systems, there are twenty-two pair interactions between absorbing and back-scattering atoms with their nearest-neighbor sites, except for the absorber and back-scatterer themselves. The anharmonic effective potential  $V_{eff}(x)$  for FCC and HCP crystals can be clearly re-written as

$$V_{eff}(x) = \varphi(x) + 2\varphi\left(-\frac{x}{2}\right) + 8\varphi\left(-\frac{x}{4}\right) + 8\varphi\left(\frac{x}{4}\right). \quad (3)$$

Let us assume that the interaction  $\varphi(r)$  between atoms in the system can be described by the Morse potential function as follows

$$\varphi(r) = D \left\{ \exp[-2\alpha(r - r_0)] - 2 \exp[-\alpha(r - r_0)] \right\}, \quad (4)$$

where  $r_0$  is the nearest-neighbor distance in the equilibrium reference structure,  $D$  is the dissociation energy and  $\alpha$  describes the width of the pair potential. This simple pairwise potential function has been extensively used because of its many advantages. For example, it accounts for the anharmonicity of real bonds, and it also includes the effects of bond breaking.

By making the Taylor expansion of this potential up to the third order of the deviation of instantaneous bond length  $x = r - r_0$ , we have

$$\varphi(x) \approx D(-1 + \alpha^2 x^2 - \alpha^3 x^3). \quad (5)$$

Substituting Eq. (5) into Eq. (3) we obtain the force constants of FCC and HCP crystals in terms of Morse potential parameters as follows

$$k_{eff}^0 = 5D\alpha^2; \quad k_3^0 = -\frac{3}{4}D\alpha^3. \quad (6)$$

### 2.2. Thermodynamic properties of AB alloys

Let us consider substitutional AB alloys in which A atoms composing the metallic A crystal are substituted by B atoms. The Morse potential parameters  $D_{AB}$  and  $\alpha_{AB}$  for A–B interactions can be derived approximately as

$$D_{AB} = \frac{1}{2}(D_A + D_B); \quad \alpha_{AB}^2 = \frac{D_A \alpha_A^2 + D_B \alpha_B^2}{D_A + D_B}. \quad (7)$$

Denoting the concentration of A and B in A–B alloys, respectively, by  $X_A$  and  $X_B$ , we have  $0 \leq X_A, X_B \leq 1$  and  $X_A + X_B = 1$ . For the simplicity of building the model, we assume  $X_A \geq X_B$ . Due to the fact that the interatomic effective potential  $V_{eff}$  of A–B alloys is contributed by both A–B and A–A pairs, we estimate the potential  $V_{eff}$  roughly as

$$V_{eff} = 2X_B V_{eff}^{AB} + (X_A - X_B) V_{eff}^A, \quad (8)$$

where  $V_{eff}^{AB}$  and  $V_{eff}^A$  are, correspondingly, the effective potential between A and B atoms, and between A atoms.

From Eqs. (2) & (8), we derive the bond-stretching force constants  $k_{eff}$  and  $k_3$  of AB alloy as

$$k_{eff} = 2X_B k_{eff}^{AB} + (X_A - X_B) k_{eff}^A, \quad (9) \\ k_3 = 2X_B k_3^{AB} + (X_A - X_B) k_3^A,$$

where  $k_{eff}^A$  and  $k_3^A$  are the force constants derived for FCC A crystal as

$$k_{eff}^A = 5D_A \alpha_A^2; \quad k_3^A = -\frac{3}{4} D_A \alpha_A^3, \quad (10)$$

and  $k_{eff}^{AB}$  and  $k_3^{AB}$  are derived from the interatomic effective potential  $V_{eff}^{AB}$  between A and B atoms

$$k_{eff}^{AB} = \left[ 1 + 8(\mu_A^2 + \mu_B^2) \right] D_{AB} \alpha_{AB}^2; \quad (11) \\ k_3^{AB} = -\left[ 1 - \mu_A^3 - \mu_B^3 \right] D_{AB} \alpha_{AB}^3,$$

with

$$\mu_A = \frac{M_A}{M_A + M_B}, \quad \mu_B = \frac{M_B}{M_A + M_B}. \quad (12)$$

The Einstein frequency and Einstein temperature of alloy system can be obtained, respectively, as [17]

$$\omega_E = \sqrt{\frac{k_{eff}}{\mu}}; \quad \theta_E = \frac{\hbar \omega_E}{k_B}, \quad (13)$$

where  $\mu$  is the reduced mass in ACEM model

$$\mu = 2X_B \mu_{AB} + (X_A - X_B) \mu_{AA}, \quad (14)$$

$$\text{and } \mu_{AB} = \frac{M_A M_B}{M_A + M_B}, \quad \mu_{AA} = \frac{M_A}{2}.$$

And the second EXAFS cumulant of AB alloy in ACEM [17] is derived as

$$\sigma^2 = \left\langle (x - \langle x \rangle)^2 \right\rangle = \frac{\hbar \omega_E}{2k_{eff}} \frac{1+z}{1-z} = \sigma_0^{(2)} \frac{1+z}{1-z}, \quad (15)$$

where  $z = \exp(-\hbar \omega_E / k_B T)$ ,  $k_B$  is the Boltzmann constant and  $\sigma_0^{(2)} = \frac{\hbar \omega_E}{2k_{eff}}$  is the zero-point contribution to the second cumulant.

**Table 1**  
The Morse potential parameters of Cu–Cu, Co–Co and Cu–Co interactions.

Bond	$D$ (Å)	$\alpha$ (eV)	$r_0$ (Å <sup>-1</sup> )	Ref.
Cu–Cu	0.3429	1.3588	2.8660	[20]
Co–Co	0.4200	1.3800	2.8000	[21]
Cu–Co	0.3814	1.3705	2.8330	Calculated

**Table 2**  
The bond-stretching force constants  $k_{eff}$ ,  $k_3$ , Einstein frequency  $\omega_E$  and Einstein temperature  $\theta_E$ , and zero-point contribution  $\sigma_0^2$  to the EXAFS DWF derived from developed ACEM.

		$k_{eff}$ (eV/Å <sup>2</sup> )	$\omega_E$ ( $\times 10^{13}$ Hz)	$\theta_E$ (K)	$\sigma_0^2$ ( $\times 10^{-4}$ Å <sup>2</sup> )
Cu	Present	3.166	3.10	237.05	32.29
	Exp. [22]	$3.12 \pm 0.06$	–	233	$36 \pm 2$
Cu <sub>90</sub> Co <sub>10</sub>	Present	3.25	3.16	241.10	31.99
	Exp. [22]	$3.81 \pm 0.06$	–	269	$32 \pm 1$
Cu <sub>80</sub> Co <sub>20</sub>	Present	3.33	3.21	245.13	31.71
	Exp.	–	–	–	–
Cu <sub>70</sub> Co <sub>30</sub>	Present	3.42	3.26	249.16	31.44
	Exp.	–	–	–	–
Cu <sub>60</sub> Co <sub>40</sub>	Present	3.50	3.31	253.19	31.18
	Exp.	–	–	–	–
Cu <sub>50</sub> Co <sub>50</sub>	Present	3.59	3.37	257.21	30.93
	Exp.	–	–	–	–
Cu <sub>40</sub> Co <sub>60</sub>	Present	3.67	3.42	261.24	30.69
	Exp.	–	–	–	–
Cu <sub>30</sub> Co <sub>70</sub>	Present	3.75	3.47	265.27	30.47
	Exp.	–	–	–	–
Cu <sub>20</sub> Co <sub>80</sub>	Present	3.84	3.52	269.30	30.25
	Exp.	–	–	–	–
Cu <sub>10</sub> Co <sub>90</sub>	Present	3.92	3.58	273.33	30.05
	Exp.	–	–	–	–
Co	Present	3.999	3.62	276.68	29.84
	Exp. [22]	$4.31 \pm 0.06$	–	285	$30 \pm 1$

### 3. Numerical calculations and discussion

In this section, numerical calculations are performed for CuCo alloys with various concentrations of Co element. The Morse potential parameters of Cu–Cu, Co–Co and Cu–Co interactions are shown in Table 1. [20,21]

Applying the developed ACEM, the force constants, the Einstein frequency and temperature of Cu, Co metals and CuCo alloys are derived. We list these calculated thermodynamic quantities in the Table 2. As we can observe from this table, the values of Einstein temperature of Cu, Co metals and CuCo alloys in our calculations are reasonably consistent with the ones derived from the fitting Einstein model with EXAFS measurements [22]. The difference between our calculated result and the measured one of Einstein temperature is about 2%–3% for metals and about 10% for Cu<sub>90</sub>Co<sub>10</sub> alloy. Here it should be noted that the Einstein temperature is a significant physical quantity derived in within view of the Einstein model. It could be seen as a rough threshold temperature so that at a higher temperature, classical considerations for thermodynamic properties of solids can be applicable. The Einstein temperature of Co metal is higher than one of Cu. This is due to the smaller effective force constant  $k_{eff}$  obtained for Cu metal in comparison with bulk Co as we can see from Eq. (12). It reflects the fact that Cu–Cu bonds are softer than Co–Co bonds. It causes a phenomenon that Cu lattice shows a greater thermal disorder. As we can see in the following, the greater thermal disorder in Cu system is equivalent to the higher parallel MSRD of bulk Cu comparing to Co metal.

Using the calculated effective force constants  $k_{eff}$  and Einstein temperatures  $\omega_E$ , we derive the values of second cumulants of Cu and Co metals at functions of temperature. In Figs. 1 & 2, we present our theoretical calculations along with experimental measurements of

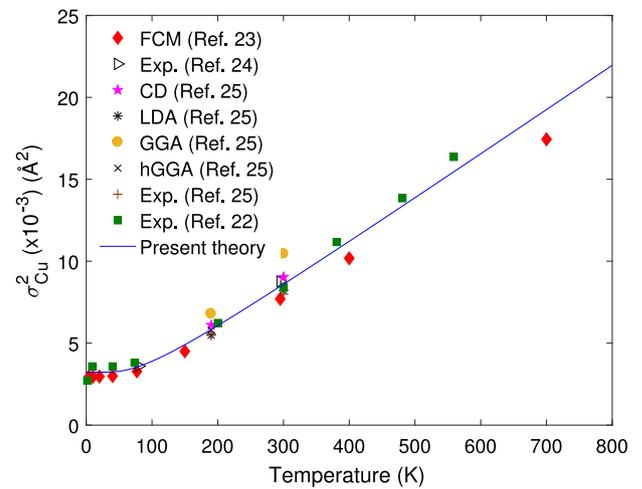


Fig. 1. (Color online) Temperature dependence of the second cumulant of Cu metal. Previous experimental measurements and theoretical calculations are shown for comparison [22–25].

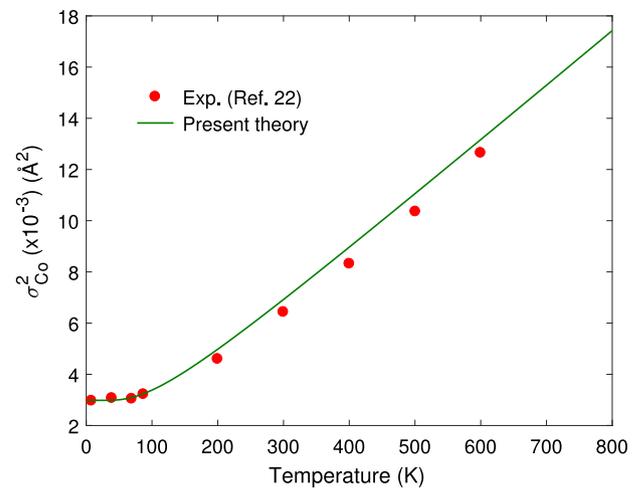


Fig. 2. (Color online) Temperature dependence of the second cumulant of Co metal. Experimental measurements are shown for comparison [22].

MSRDs of Cu and Co metals, respectively, up to temperature 800 K. As it can be seen from these two figures, the DWFs derived from ACEM are in good agreement with available experimental measurements and theoretical calculations for both Cu and Co metals [22–25]. It confirms the ACEM is reliable and applicable to investigate the temperature-dependent EXAFS DWF of metals. We can realize that the DWF is an increasing function of temperature, and above 150 K, it is the almost linear proportion to temperature. The slopes of DWF curves  $d\sigma^2/dT$  in temperature region beyond 150 K of Cu and Co metals are, respectively,  $2.62 \times 10^{-5}$  Å<sup>2</sup>/K and  $2.05 \times 10^{-5}$  Å<sup>2</sup>/K. The rapid increasing of DWF function shows the significant contributions of thermal disorder at high temperature.

The temperature dependence of second cumulants of CuCo alloys with various Co concentration is shown in Fig. 3. As we can see from this figure, the parallel MSRD of CuCo alloys increases with the increasing of Co concentration. This effect can be explained as follows: When Cu atoms are substituted by Co atoms in the Cu matrix, the dispersed Co atoms will be bound to Cu atoms with stiffer bonds compared to Cu–Cu interactions. As a result, CuCo alloys show a weaker thermal disorder (corresponding to lower DWF) comparing to Cu metals. Numerically, the theoretical slopes of DWF curves  $d\sigma^2/dT$  in temperature region beyond 200 K of Cu<sub>90</sub>Co<sub>10</sub>, Cu<sub>50</sub>Co<sub>50</sub> and Cu<sub>10</sub>Co<sub>90</sub> alloys are

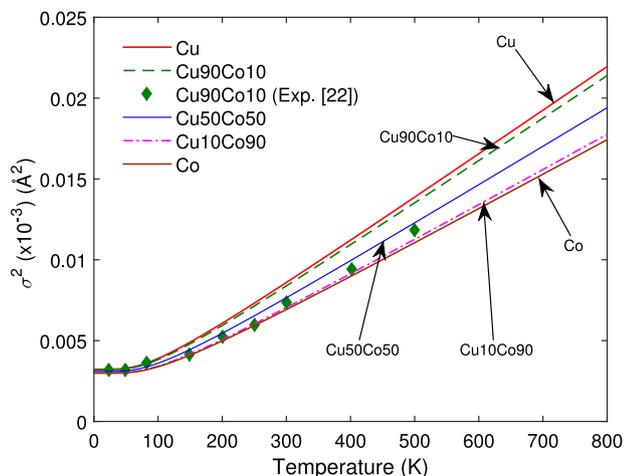


Fig. 3. (Color online) Temperature dependence of the second cumulant of CuCo alloys with various Co concentration. Experimental measurements are shown for comparison [22].

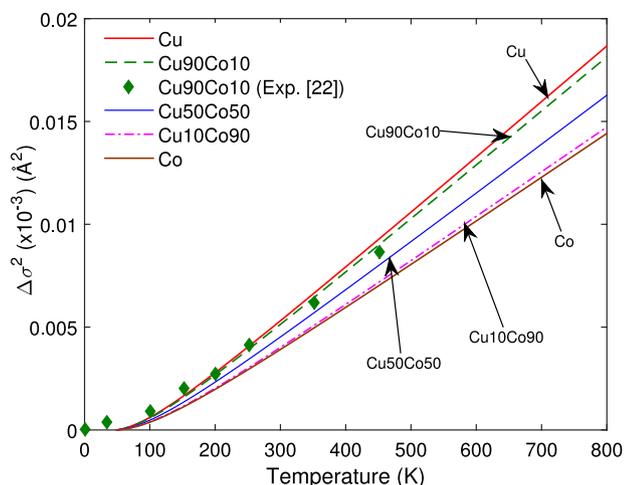


Fig. 4. (Color online) The change of second cumulant of CuCo alloys relative to the reference at temperature of 50 K. Experimental measurements are shown for comparison [22].

predicted, respectively, as  $2.55 \times 10^{-5} \text{ \AA}^2/\text{K}$ ,  $2.30 \times 10^{-5} \text{ \AA}^2/\text{K}$  and  $2.09 \times 10^{-5} \text{ \AA}^2/\text{K}$ . Moreover, our EXAFS DWF results of  $\text{Cu}_{90}\text{Co}_{10}$  (dashed line) overestimate the experimental EXAFS measurements by Cezar et al. [22] (closed diamond symbols). This phenomenon originates from the nature of EXAFS DWF as explained in the next paragraph.

It is worth to mentioning that the second cumulant  $\sigma^2$  corresponds to the parallel atomic MSRD characterizing the EXAFS Debye–Waller factor. It includes both the static disorder and thermal disorder. The first contribution is so-called structural disorder which is caused by strain or alloying. Meanwhile, the thermal disorder is dynamic disorder originated from the thermal lattice vibrations. It provides information of bond-stretching force constants between pair absorber–backscatterer atoms which correspond to the dynamical properties of them [26]. For this reason, if we calculate the change of EXAFS DWF relative to the one at a reference temperature, we can eliminate errors in calculation of the static disorder. In Fig. 4, we show the relative change of the EXAFS DWF to the reference at temperature of 50 K denoted by  $\Delta\sigma^2$  (in  $10^{-3} \text{ \AA}^2$ ). As observed from this figure, after removing the structural disorder, our theoretical prediction of EXAFS DWF change of  $\text{Cu}_{90}\text{Co}_{10}$  alloy is in good agreement with measurement of Cezar et al. [22] (closed diamond symbols).

Before making conclusions, it should be noted that from the definition of EXAFS DWF in Eq. (1), the values of EXAFS DWFs are dependent on the MSDs of central atom, its neighboring atoms and their DCF. It means that the values of EXAFS DWFs depend on the specific local chemical order. Therefore, theoretically, we are able to differentiate between ideal substitutional solid solution and solid solution with an explicit local chemical order based on temperature trends of EXAFS DWFs.

#### 4. Conclusions

We have investigated thermodynamic properties of CuCo alloys based on the developed anharmonic correlated Einstein model. Using the Morse potential, numerical calculations have been performed to derive the bond-stretching force constants, Einstein frequency and temperature and mean-square relative displacement of CuCo alloys up to temperature 800 K with various Co concentration. Our research shows that Co–Co bonds are stiffer than Cu–Cu bonds. This leads to the weaker thermal disorder in CuCo alloys in comparison to Cu metal. Furthermore, the dynamic disorder due to thermal lattice vibrations is significant to the EXAFS DWF at high temperature. The reasonable agreement between our theoretical prediction and previous measurements shows that the developed ACEM is applicable to investigate thermodynamic properties of alloys in EXAFS theory. The reported results increase the database of the Einstein frequency and corresponding temperature, and the mean-square relative displacement of CuCo alloys. These data can be used to verify future EXAFS experiments.

#### CRediT authorship contribution statement

**Pham Thi Minh Hanh:** Data curation, Formal analysis, Investigation, Methodology, Writing - original draft, Writing - review & editing. **Nguyen Ba Duc:** Resources, Project administration, Funding acquisition, Supervision, Investigation, Writing - original draft, Writing - review & editing. **Nguyen Van Nghia:** Validation, Writing - review & editing. **Nguyen Viet Tuyen:** Validation, Visualization, Writing - review & editing. **Ho Khac Hieu:** Conceptualization, Resources, Validation, Writing - original draft, Writing - review & editing.

#### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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